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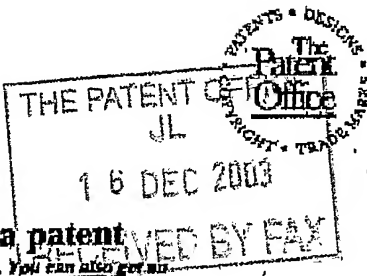
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Renishaw plc
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Patents ADP number (if you know it)

2691002

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4. Title of the invention

Method Of Calibrating A
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METHOD OF CALIBRATING A SCANNING SYSTEM.

The present invention relates to a method of calibrating a scanning system. A scanning system in this specification should be understood to mean a combination of a machine and a probe which together are capable of use in scanning an object in order to obtain information about its size, shape or surface contours.

10 The machine may be, for example, a co-ordinate measuring machine (CMM), machine tool or robot etc, and the probe is a measuring probe with a workpiece-contacting stylus. One type of machine has measuring devices for measuring the movement of the machine parts in three nominally orthogonal directions (referred to as X, Y and Z axes), and one type of probe includes measuring transducers for producing outputs indicative of the displacement of the tip of the stylus relative to the probe in three nominally orthogonal directions (referred to as the a, b, and c axes). Although the term 'analogue probe' is used, the outputs for the a, b and c axes may be either analogue or digital.

25 In known systems, measurement errors are caused by unwanted deflections of the probe, machine structure and workpiece. Errors due to bending of the probe stylus are the same throughout the machine volume and may be compensated for by probe calibration. Errors due to deflections in the machine structure may be caused, for example, by the machine quill bending and the machine bridge twisting and vary throughout the machine volume. These errors increase, for example, with increasing cantilevers. Errors in the object to be measured may be caused by object deflection during

measurement as a result of force by the probe.

Parts of the working volume of the machine may be calibrated for measurement errors by using a calibration artefact such as a calibration sphere. However usually the calibration artefact cannot be located at the same position in the machine's working volume as the part to be measured and is instead located to one side. The measurement errors determined at the calibration artefact will thus be different to those on the part.

Methods of correcting machines for acceleration induced errors are known. One example of such a method is described in European Patent No. 318557. In this method a first article from a batch of nominally identical articles is measured at a relatively slow speed, noting the measurements of the positions of a number of datum points on the article. The measurement operation is repeated at a relatively fast speed noting the measurements of the positions of the same datum points. Any difference in the measurements are noted as errors in a correction table.

Thereafter all of the articles are measured at the relatively fast speed taking measurements of the positions of corresponding points on each article, and these measurements are corrected for machine accelerations using the previously noted errors.

Another method of correcting errors is disclosed in WO00/62015. In this method a stylus of a probe mounted on a coordinate measuring machine is driven into contact with a surface of an object in a direction

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normal to its surface until a predetermined stylus deflection has been reached. The machine is then reversed whilst simultaneously recording the outputs of the machine measuring devices and measuring transducers of the probe. This process is repeated for a selection of datum points around the surface of the object. The measurements for each datum points are extrapolated to determine the measurement which would have been taken when the probe deflection is zero. This extrapolated value relates to when the probe is just in contact with the surface.

The object is then scanned at a slow speed and predetermined stylus deflection. The difference at the datum points between the initial measurements and the scan is recorded.

The scans are repeated at the same stylus deflection at greater speeds until the variation in the recorded differences between the fast scan and the initial measurements and the slow scan and the initial measurements exceeds a defined tolerance. The last speed which falls within this tolerance is the maximum scanning speed. A map of the positional errors at the datum points is stored along with the data relating to the scanning speed, particular artefact, particular CMM and probe and stylus configuration etc. It is possible to interpolate from this map to obtain radial errors at angles in between the radial directions at which actual data was obtained (i.e. the datum points).

This method has the disadvantage that the step of collecting the datum points is time consuming.

The present invention provides a method of measuring an object on a coordinate positioning apparatus, comprising the following steps, in any suitable order:

5 placing the object on the coordinate positioning apparatus;

measuring the object with a workpiece contacting probe to create measurement data of the object, the measurement data being collected at multiple stylus deflections or probe forces;

10 for at least one location on the surface of the object, determining a function relating the measurement error data to the stylus deflection or probe force;

for said at least one location on the surface of the object, using the function to determine the measurement data corresponding to zero stylus deflection or zero probe force;

15 and outputting the measurement data corresponding to zero stylus deflection or zero probe force as the measurement of the object.

20

The term measuring includes taking measurements using either a scanning probe or a touch trigger probe.

25 The known stylus deflection or probe force may be a known constant deflection or force or a known varying deflection or force.

30 Preferably the step of measuring the object with a workpiece contacting probe comprises scanning the object.

The function may be a linear function. The function may be a parametric function.

5

In one embodiment, the object is measured along a scan path and measurement data is collected at multiple stylus deflections or probe forces for a section of the scan path;

- 5 the function relating the measurement data to the stylus deflection or probe force is determined for locations on said section of the scan path;

- and wherein for locations on the scan path but not on said section of the scan path, the function relating
10 the measurement data to the stylus deflection or probe force is determined from measurement data collected on said section of the scan path.

- The function relating the measurement data to the
15 stylus deflection or probe force for locations on the scan path but not on said section of the scan path is determined from the X and Y axis components of the function relating the measurement data to the stylus deflection or probe force on said section of the scan.
20 path.

- The object may be measured along the scan path by scanning a surface profile for one revolution at a constant or variable probe deflection or probe force.
25 Measurement data may be collected at multiple stylus deflections or probe forces for a section of the scan path by taking additional measurements on the scan path at a different probe deflection or probe force. The additional measurements may be taken by scanning the
30 surface profile for at least a quarter revolution. Alternatively, the measurements may be taken by taking measurements of the surface profile as the probe is moved radially towards or away from the surface at at least two different locations.

Preferred embodiments of the invention will now be described with reference to the accompanying drawings in which:

Fig 1 is a schematic diagram of an analogue probe
5 mounted on a coordinate measuring machine;

Fig 2 is a schematic representation of several different constant stylus deflection scans around an object;

Fig 3 is a graph illustrating probe deflection
10 against object diameter;

Fig 4 is a graph illustrating probe force against probe deflection;

Fig 5 is a graph illustrating the radial error against probe deflection

Fig 6 is a schematic illustration of the static correction vectors;
15

Fig 7 is a schematic representation of several different constant force scans around an object;

Figs 8-10 are schematic illustrations of a feature
20 being deflected under measurement force;

Fig 11 illustrates the real diameter and the measured diameter of a feature having low stiffness;

Fig 12 is a schematic illustration of the dynamic correction vectors;

Fig 13 illustrates the scan profiles during the method of a second embodiment of the invention;
25

Fig 14 shows a portion of the scan profiles of Fig 13;

Fig 15 illustrates a workpiece being measured
30 according to a third embodiment of the invention;

Fig 16 is a schematic representation of a scan with a sinusoidally varying stylus deflection around an object;

Fig 17 is a schematic representation of a scan

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with a single sinusoidally varying stylus deflection around an object;

Fig 18 illustrates a section of the scan profile of Fig 17;

5 Fig 19 illustrates a graph of a function relating part measurement R and probe force F;

Fig 20 illustrates a bore being scanned using the scan profile shown in either of figs 21 or 22;

10 Fig 21 illustrates a scan profile in which a bore is scanned a complete revolution and a quarter revolution;

Fig 22 illustrates a scan profile in which a bore is scanned a complete revolution and then radially at two locations; and

15 Fig 23 is a graph illustrating a radial measurement used in the scan profile of Fig 22;

In a first step of the invention, a measurement force error map is generated for an object. This is achieved
20 by mounting an analogue probe 10 on the quill 12 of a coordinate measuring machine (CMM) (not shown) as illustrated in Fig 1. The analogue probe 10 has a deflectable stylus 14 with a workpiece contacting tip 16. The object 18 to be measured is mounted on the CMM
25 machine table 20 and the probe 10 is driven slowly by the machine quill 12 in a path around the object. The object 18 is first scanned along a path at a first constant probe deflection, for example 300µm. The object is then scanned along this path at one or more
30 different subsequent probe deflections. For example, the part may be scanned a second time with a probe deflection of 200µm and a third time with a probe deflection of 100µm. Fig 2 shows a representation of the object 18 and the measurements obtained from the

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first 22, second 24 and third 26 scans around it. Each point on the object 18 will thus have three different measurements A,B,C, resulting from the three different scans at different probe deflections. For each point
5 on the object, the measurements may be extrapolated back to calculate the measurement which would have been taken if the probe deflection was zero. Fig 3 shows a graph of the probe deflection against object diameter. The actual object diameter is shown at zero probe
10 deflection. The step of extrapolating to zero probe deflection allows the measurements at zero probe deflection to be determined without the errors of actual measurement, caused by probing force errors. A passive probe is suitable for use in this method, such
15 a probe may comprise a stylus deflectable against springs.

This information enables a measurement force error map of the part to be produced. If the scans of the part
20 were taken at a slow speed, this results in negligible dynamic errors due to very low accelerations of the probe and machine.

Fig 4 shows the relationship of probe force against
25 probe deflection. The probe acts within Hook's law such that when there is zero probe force, there is zero probe deflection.

Fig 5 illustrates the relationship of radial error
30 against probe deflection. Points A,B and C relate to the radial error at probe deflection 100µm, 200µm and 300µm respectively. By using these points to extrapolate to zero probe deflection, zero radial error is achieved. Once the function relating probe

deflection and radial error has been determined, a subsequent measurement taken at any probe deflection, for example point P, may be corrected to zero radial error using this function. As there is a linear
5 relationship between probe deflection and radial error, the function for correcting measurements at a given probe deflection is also linear.

Alternatively the measurement force error may be in the
10 form of an error map. This could be in the form of a look-up table, with different error corrections for different stylus deflections. The error map could be in the form of a polynomial function.

15 Fig 6 shows the error corrections for points on the scan. Each point on the scan has a different radial correction 38 which is applied for a certain stylus deflection. If a subsequent object is scanned at a stylus deflection of 300µm 36, the measurement force
20 error function or map may be used to correct the measured dimensions 36 taken at this stylus deflection to the actual part dimensions 34 corresponding to the part being scanned at a deflection of 0µm.

25 This method is not limited to each scan having a constant deflection, as long as points on the object surface have measurement data corresponding to different stylus deflections to enable the measurement data to be extrapolated to zero. For example, Fig 16
30 illustrates a first scan profile 60 around an object 18 taken at constant deflection and a second scan profile 62 taken using a sinusoidally varying deflection. Points P1, P2, P3 on the object surface thus each have two measurements taken at different probe deflections.

10

This measurement data may be extrapolated to zero as previously described.

It is also possible to collect sufficient measurement data during a single varying scan profile. Fig 17 illustrates a single scan profile 70 around an object 18, the scan profile 70 being taken using a sinusoidally varying stylus deflection. Fig 18 illustrates a section of the scan profile 70. Over a small angle 72, scan profile 70 contains many data points taken at different stylus deflections. Assuming changes in the surface are small over angle 72 (eg part deflection and uniformity of surface), these data points taken at different stylus deflections over angle 72 may be used for the extrapolation to zero calculation. This is also possible if there is a change in the surface profile over angle 72, as long as the change can be assumed to be linear.

Alternatively, instead of scanning the object several times at different probe deflections, it may be scanned several times with the probe having a different constant force for each scan. For example, the object may be first scanned with a constant force between the stylus and the object of 0.3N. The object may then be scanned a second time with a constant force of 0.2N and a third time with a constant force of 0.1N. Each of these scans may have the same or different stylus deflections. Fig 7 shows a representation of the object 18 with an actual part dimension 34 and the measured dimensions obtained from the first 28, second 30 and third 32 scans at different constant probe forces.

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- As before, for a point on the surface of the object, there are three sets of data relating to the scans at different probe forces. This data may be extrapolated back to enable the point which would be measured with
- 5 zero force between the stylus and workpiece (i.e. the actual part dimensions) to be determined. As described previously, an error function or map may be created relating measurements taken at a given probe force to the correct measurements for a given point determined
- 10 for zero probe force by the extrapolating to zero technique. Subsequent measurements at a given probe force may be corrected for measurement force errors using this measurement error function or map.
- 15 As with the previous method, sufficient data may be collected from a single scan of varying probe force (eg having a sinusoidal profile) to do the extrapolate to zero calculation.
- 20 This method is suitable for use in an active scanning probe, in which a motorised mechanism is used to control and modulate the contact force with the component to be measured.
- 25 The object may comprise a part of a series of parts to be measured. In this case a measurement force error map of this part is produced by this method. Alternatively, the object may comprise an artefact having features corresponding to the features on the
- 30 parts to be subsequently measured. These features may be, for example, spheres, ring gauges, plug gauges etc. Use of the artefact allows geometric errors in addition to the probing force measurement errors, to be determined. Geometric errors are errors of the machine

- and probe, for example non-linearity of the machine scales or the machine axes not being straight. As the forms of the features on the artefact are known, they may be used to correct for geometric errors of the machine and probe. This may be done by comparing the extrapolated to zero data of the artefact with the known form of the artefact and producing a geometric error map to correct subsequent parts with. This method may also be used to directly measure a part, without first creating an error map.
- As previously described, a first measurement R_1 of the part is obtained at a first probe deflection or probe force F_1 and a second measurement R_2 of the part is obtained at a second probe deflection or probe force F_2 . This may be repeated for subsequent measurements R_n at different probe deflections or probe forces F_n . A function relating measurement data of the part to the probe deflection or probe force is determined from the measurements R_1, R_2 of the part and corresponding probe deflections or probe forces F_1, F_2 . This function may be a linear or higher order curve (e.g. a parametric curve). The function is used to extrapolate the measurement data to provide the measurement data R_0 of the part relating to zero probe force F_0 . However in this embodiment, the measurement data R_0 corresponding to zero probe force is calculated "on the fly", and thus without the requirement to first calculate an error map of the part.
- Fig 19 illustrates a linear function relating part measurement R and probe force F determined from the measurement data R_1, R_2 and the corresponding probe force F_1 and F_2 . In this case, R_0 is determined by the

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equation:

$$R_0 = R_1 - \frac{(R_2 - R_1) \cdot F_1}{(F_2 - F_1)}$$

5 As described previously, at least one of the sets of measurement data may be obtained during a scan with non-constant probe deflection or probe force, for example a sinusoidal scan. Alternatively, a single scan of the part with varying probe deflection or probe
10 force may enable sufficient data to be collected for the "on the fly" extrapolation calculation.

It is not a requirement to have two complete scans of the feature to be measured. For example, Fig 20
15 illustrates a bore 80 which is being scanned by a probe 82. Fig 21 shows the scan profile of the bore, which is measured a first time 84 at a first probe deflection or force for a complete revolution. The bore is then scanned a second time 86 at a second probe deflection
20 or force for a quarter revolution. The first 84 and second 86 scans may be at constant or variable probe deflection or probe force. As in previous embodiments, the data from the first and second scans are used to determine the surface measurement at points on the bore
25 surface at zero probe force by extrapolation to zero. The data from the quarter scan 86 has sufficient information about the errors along the X and Y axes that scan data may be corrected around the whole circumference of the bore using this data.

30

The quarter scan may be replaced by two radial sets of measurements. For example Fig 22 illustrates a scan profile of the bore in Fig 20 in which the bore is

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scanned a first time 84 as before. Instead of the second quarter scan, the probe is brought radially towards and away from the surface of a bore at a first position 88, whilst taking surface measurements at different probe deflections or probe forces. Fig 23 is a graph illustrating probe deflection against surface measurement for measurements taken at a point on the bore surface as the probe is moved radially towards the bore surface. This is repeated at a second position 90 on the bore surface, spaced angularly from the first. Preferably the radial measurements are 90° apart for ease of extracting the corrections along the X and Y axes, however the radial measurements may be spaced at different angles. As before, extrapolation to zero at the two radial positions enables a true measurement relating to zero probe force to be determined at two positions. Thus the error corrections relating to X and Y may be determined and hence measurements may be corrected across the whole bore.

This method is adequate when the walls of the feature being measured are sufficient thick so that there is no significant local part deflection, which would affect the correction at local areas of the bore.

This method has the advantage that the errors due to probing force measurement errors and geometric errors can be separated. This would not be the case if, for example, measurement data from a scan with 300µm deflection is compared with the known form of the artefact. In this case the probing force measurement error and geometric error would be combined into one correction and it would not be possible to separate them.

15

This method of correcting for separate measurement force errors and geometric errors has the advantage that it takes into account the errors due to deflection of the object being measured. Objects with low stiffness and/or thin walls may deflect with the probing force whilst being measured.

Fig 8 illustrates a feature 50 to be measured which has low stiffness. When the feature is contacted with a probe 10, as shown in Figs 9 and 10, the feature deflects away from the probe. This deflection of the feature caused its diameter measured at force F to appear smaller than its actual diameter. Fig 11 illustrates the actual diameter 52 of the feature and the measured diameter 54 using a probe force F. Similarly, the inner diameter of a ring would appear larger than its actual diameter for the same reason. At zero probe deflection or zero probe force there will be zero deflection of the feature. Thus the measurement force error function or map created by the method of this invention takes account of these errors by this extrapolating to zero step.

In a second step of the invention, the dynamic errors of the system are determined. Dynamic errors may be caused, for example, by machine bending due to acceleration. Once the measurement force error function or map has been produced as described above, the object is scanned at a high speed. The high speed scan is carried out at either constant probe deflection or constant force, as above. In addition, the high speed scan is preferably performed at a constant speed. The measurement data from this fast scan is compared with the measurement force error corrected slow scan relating to the actual dimensions of the object,

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produced as described in the first step of the invention. A dynamic error function or map may be produced by comparing the fast scan and the measurement error corrected slow scan. This dynamic error map is
5 used to correct subsequent scans taken at a fast speed.

The subsequent scans do not need to have the same stylus deflection or probe force as the original fast scans as the dynamic error function relates the error
10 to the deflection or force. However, it is desirable to use a similar fast speed for the subsequent scans.

Fig 12 illustrates the measurements taken during the fast scan 40 and the actual dimension 42 of the object
15 created by measurement force error correcting the slow scan as previously described.

The dynamic error map has been combined with the measurement force error map or function to create a
20 total feature map. This is done by adding the measurement force error correction vectors 38 around the part illustrated in Fig 6 with the dynamic error correction vectors around the part to create combined
correction vectors 44 illustrated in Fig 12.

25

This method has the advantage that as the measurement errors are determined by scanning the object at different probe deflections or different forces, the measurement errors are known for every point on the
30 surface of the object. Thus no interpolation is required.

In a second embodiment of the invention, the measurement force errors and the dynamic errors may be

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determined in combination. Such a method will now be described with reference to Figs 13 and 14.

In a first step, an object is scanned at a slow speed for example 10mm/s with a first deflection, for example 200 μ m. Fig 13 shows the profile of the slow scan S1. The object is then scanned along the same path at a fast speed, for example 100mm/s and at a second deflection, for example 100 μ m. Fig 13 shows the profile of the fast scan F1. The object is then scanned along the same path at the fast speed 100mm/s and at the first deflection 200 μ m. Fig 13 shows the profile of the fast scan F2.

Fig 14 shows a portion of the S1, F1 and F2 scan profiles around the object. F1 and F2 are profiles for scans of the same fast speed (100mm/s) but different deflections (100 μ m and 200 μ m respectively). By extrapolating to zero deflection, the profile of the object for a high speed (100mm/s) scan with zero deflection can be determined. This profile is shown as HSZD on Fig 14. The error due to deflection of the F2 scan may thus be determined. This deflection error is shown as e_1 , on Fig 14.

As scans S1 and F2 were carried out with the same probe deflection (200 μ m), the deflection error e_1 may be applied to the profile of scan S1 to find the profile corresponding to a scan at low speed with zero deflection. This profile is shown as LSZD on Fig 14 and corresponds to the surface of the object.

The LSZD is now used as a base line. The error between the LSZD baseline and the F2 scan is now determined.

18

This is labelled e_2 on Fig 14. The errors e_2 may be stored as a correction map or function.

Subsequent objects may now be measured at a speed and deflection corresponding to scan F2 and corrected using the correction map or function.

This method may be used with a force-measuring probe rather than a deflection-measuring probe. In this case, scans S1 and F2 are carried out at a first probe force and scan F1 is carried out at a second probe force. The two fast scans must then be extrapolated to zero force to determine the high speed zero force profile and thus the error due to force of the F2 scan may be determined.

The measurements of the object during the S1, F1 and F2 scans may be determined by using either a scanning probe or a touch trigger probe. A touch trigger probe may be electronically loaded so that it triggers at a certain force. Thus during the S1 and F2 scans the probe is loaded to trigger at a first force and during the F1 scan the probe is loaded to trigger at a second force, enabling the two fast scans to extrapolate to zero force.

It is not necessary for the slow scan S1 to have the same stylus deflection or probe force as the fast scan F1. This is because the relationship between stylus deflection/probe force and measurement error is determined at the fast speed from scans F1 and F2, which enables comparison with any stylus deflection/probe force at the slow speed.

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A third embodiment of the invention will now be described with reference to Fig 15. A stylus 10 of a probe is driven into contact with a surface of an object 18 along a path 46 in a direction normal to the object's surface until a predetermined stylus force has been reached. This step is repeated along the same path for a plurality of different predetermined stylus forces. The measurement data along this path is used to extrapolate back to enable the point which would be measured with zero forces between the stylus and workpiece to be determined. This is the nominal object measurement.

This process is repeated for a selection of datum points around the surface of the object. The data from each of these datum points is used to create an error map as previously described to correct subsequent measurements. Measurements of the surface of the object between the datum points are corrected by interpolating the error map between the datum points.



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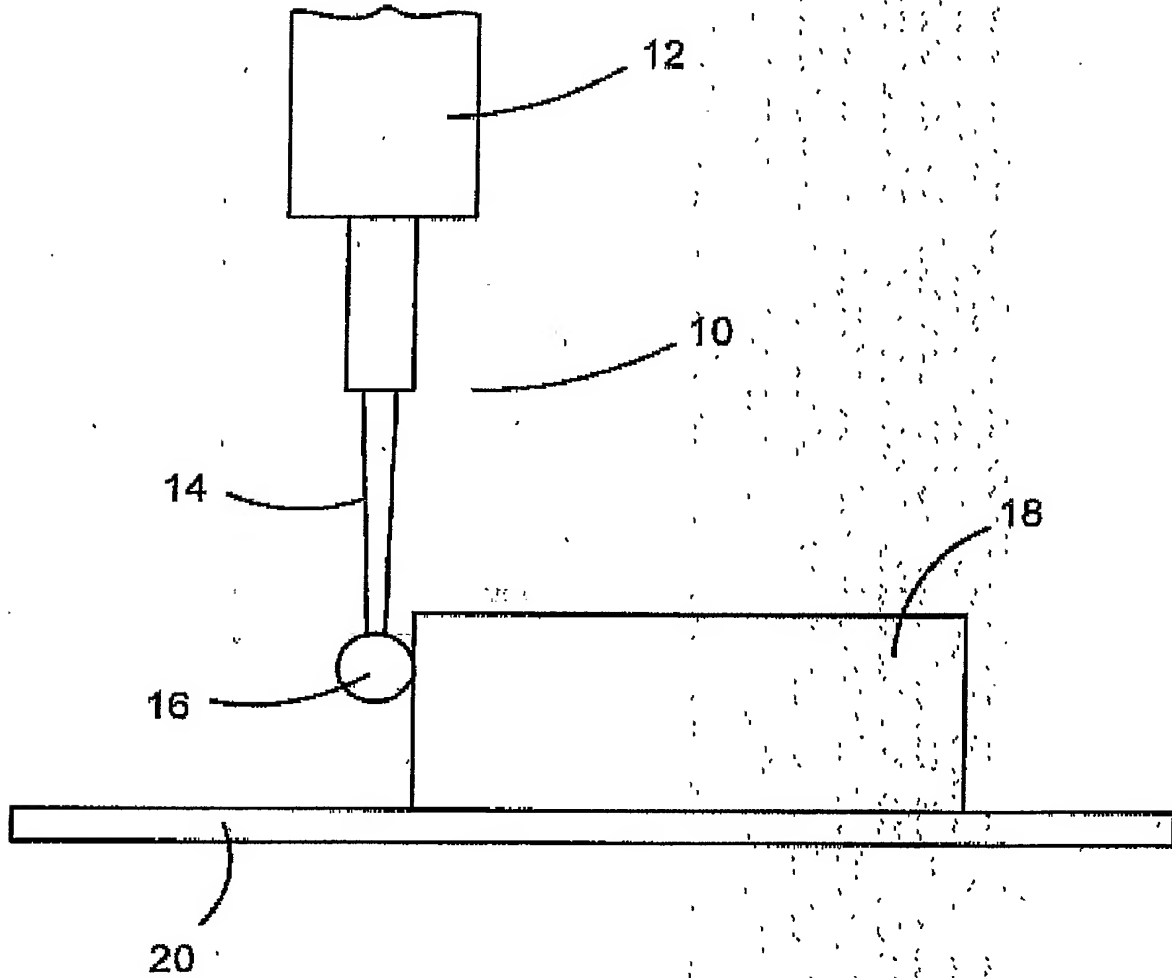


Fig 1



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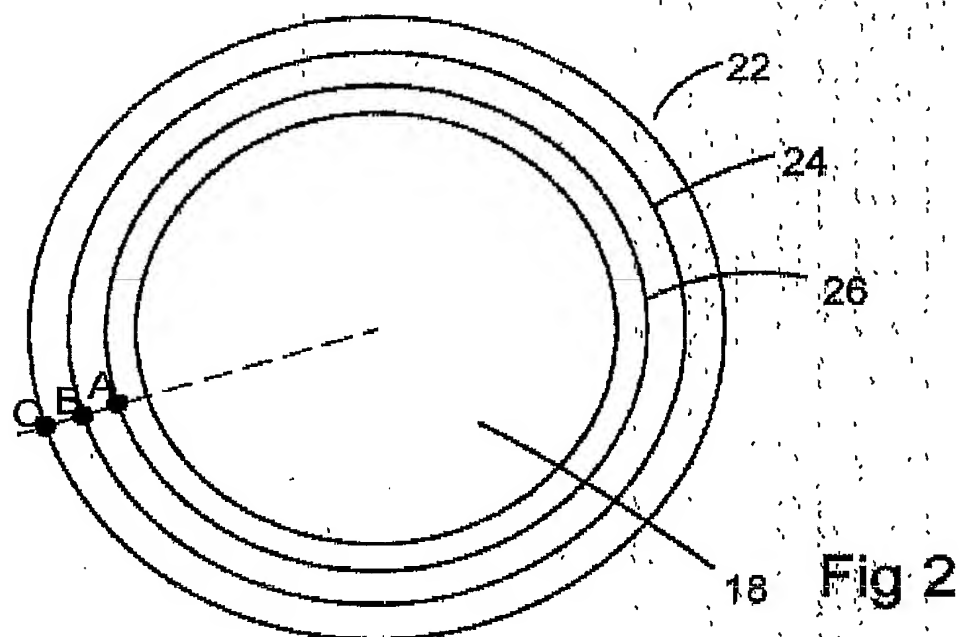
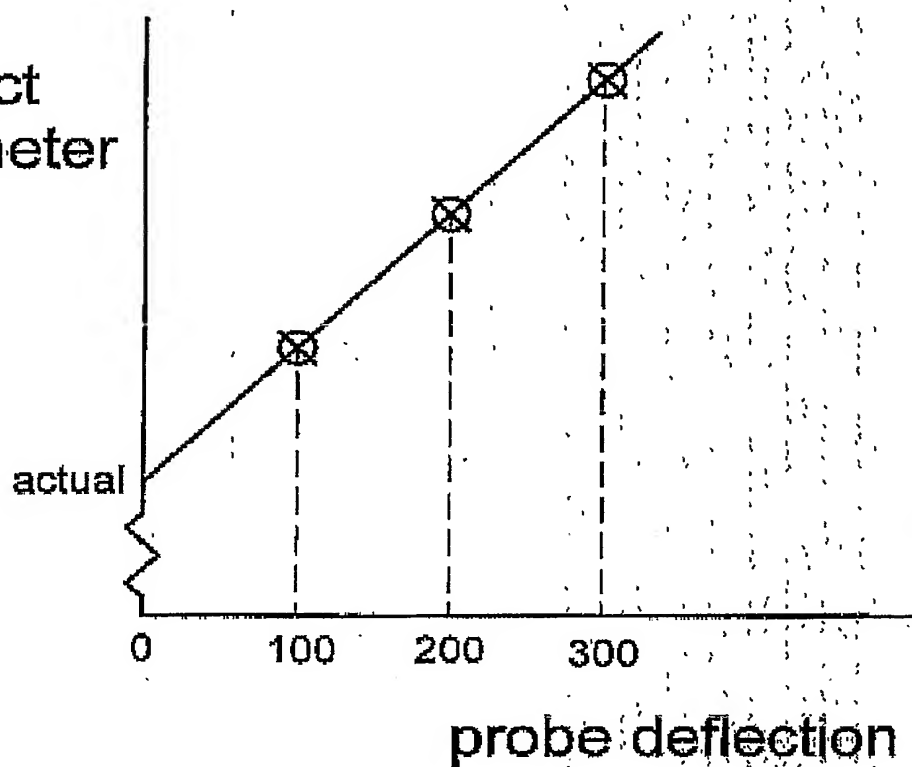
object
diameter

Fig 3



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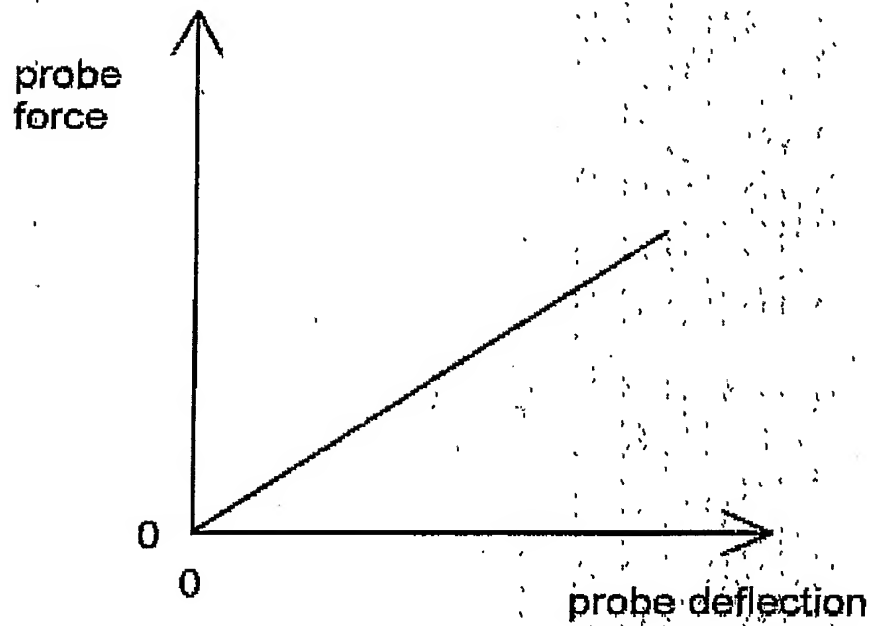


Fig 4

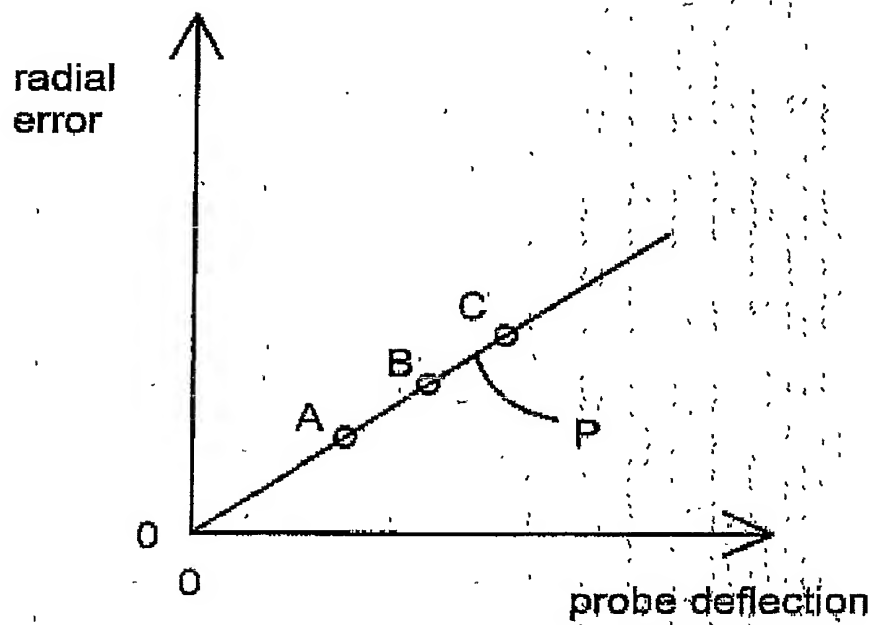
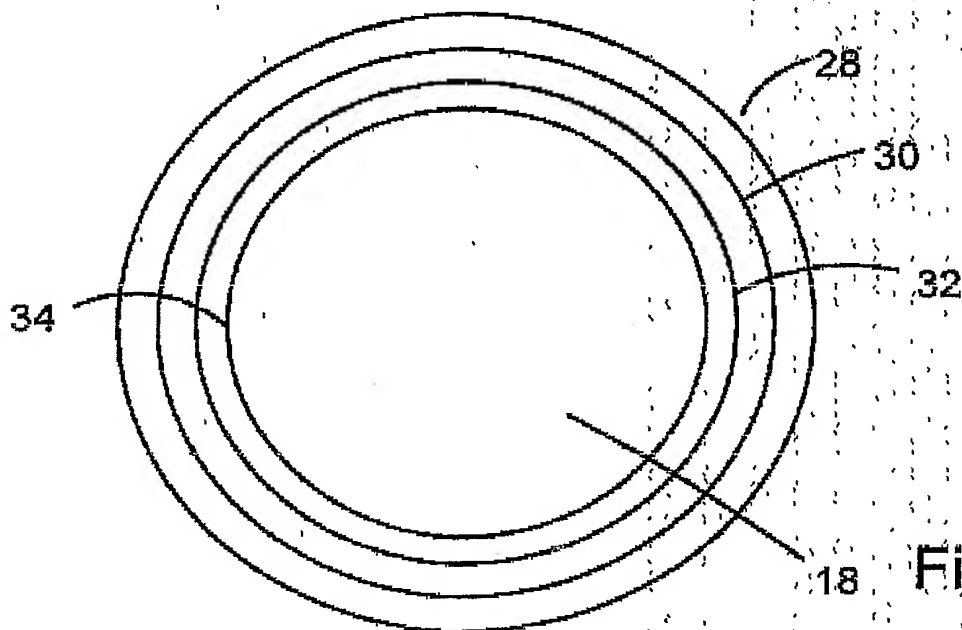
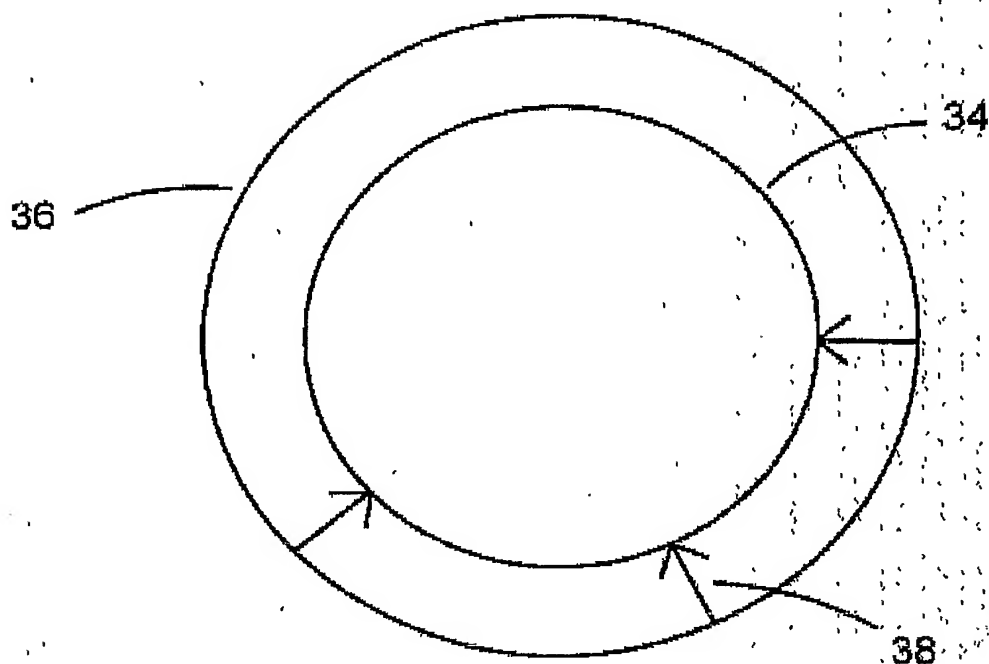


Fig 5



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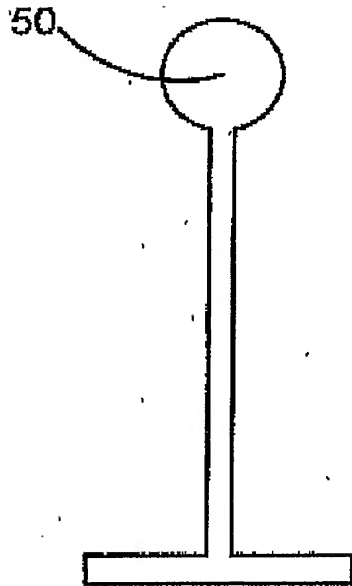


Fig 8

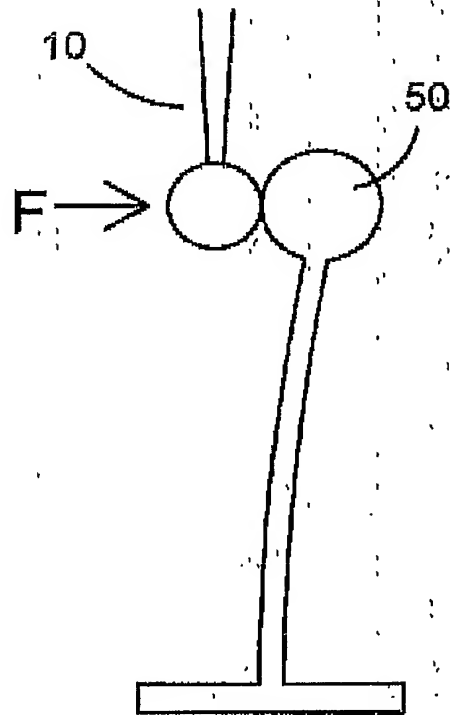


Fig 9

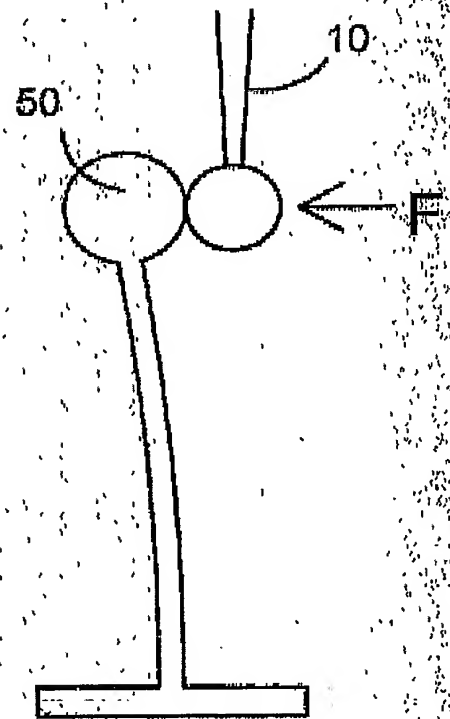


Fig 10

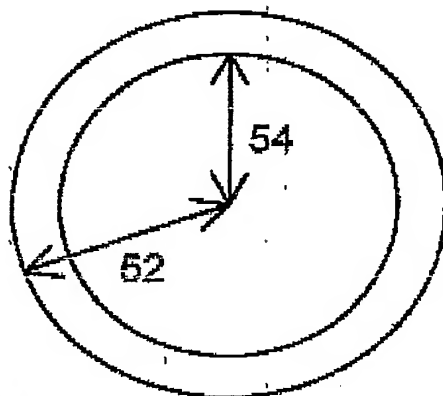


Fig 11



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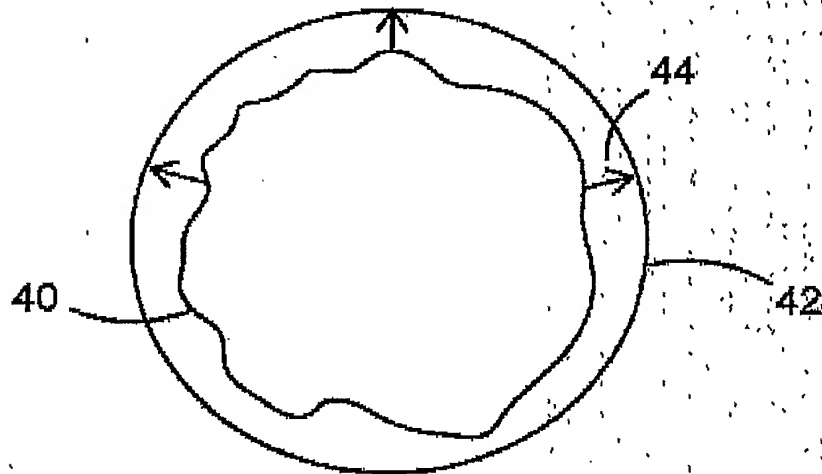


Fig 12

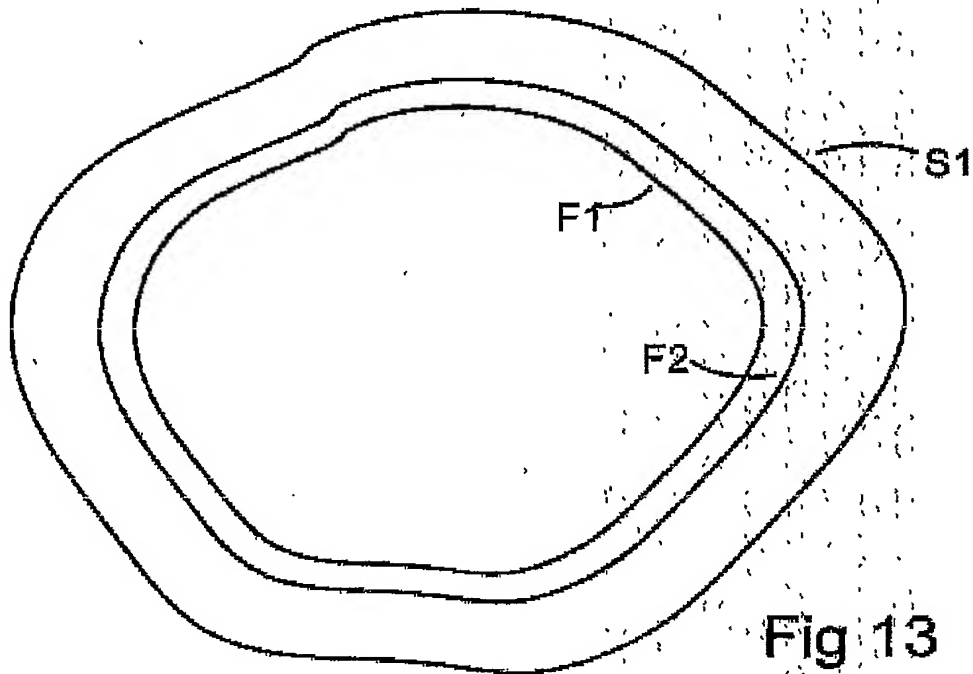


Fig 13



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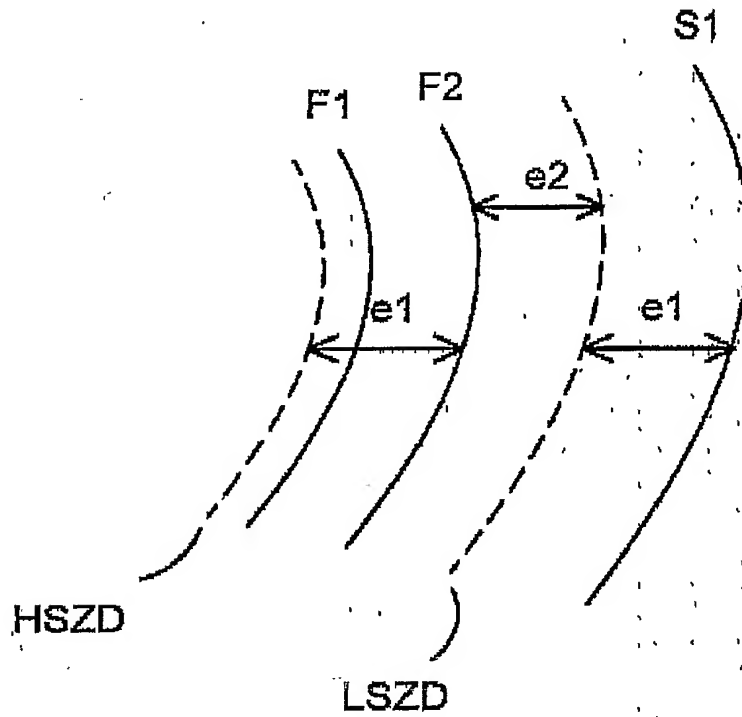


Fig 14

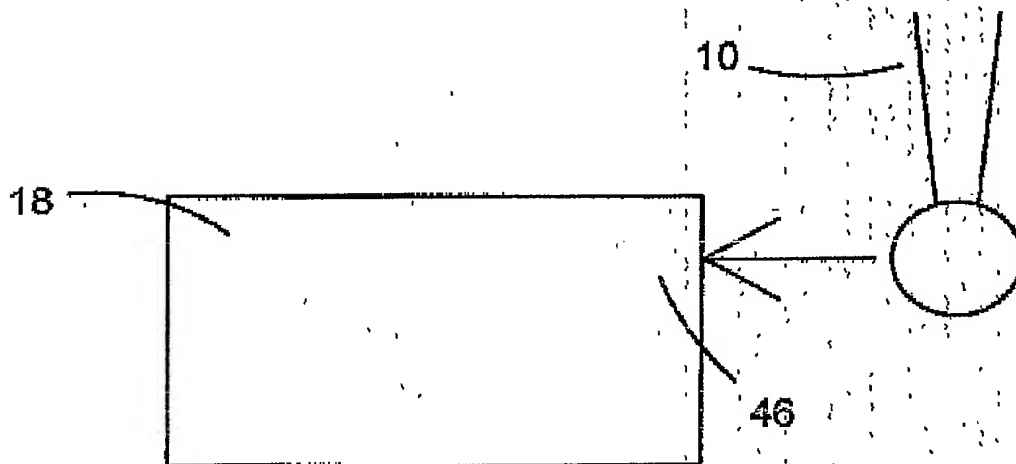


Fig 15



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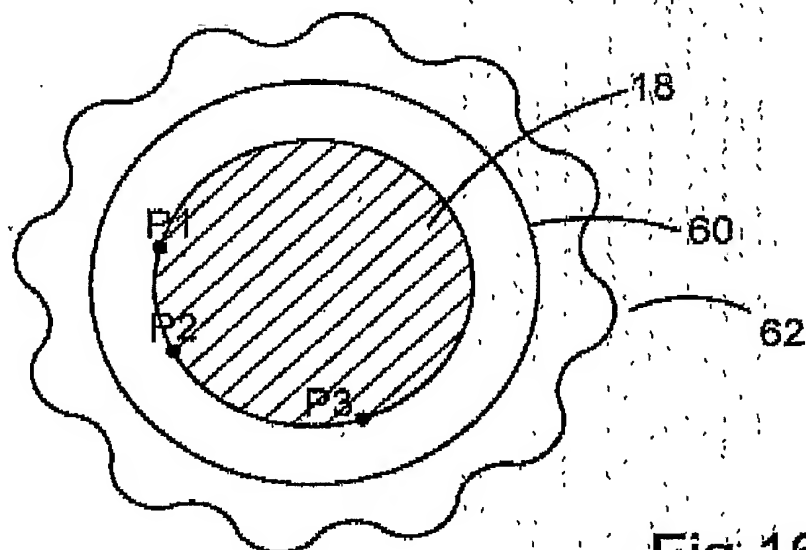


Fig 16

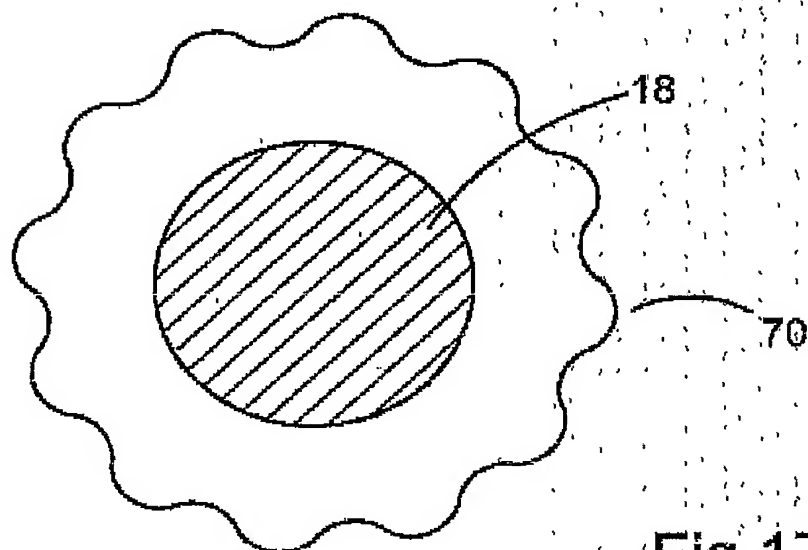


Fig 17



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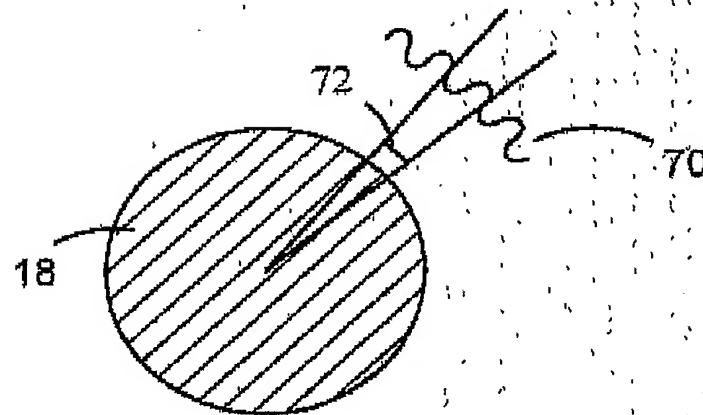


Fig 18

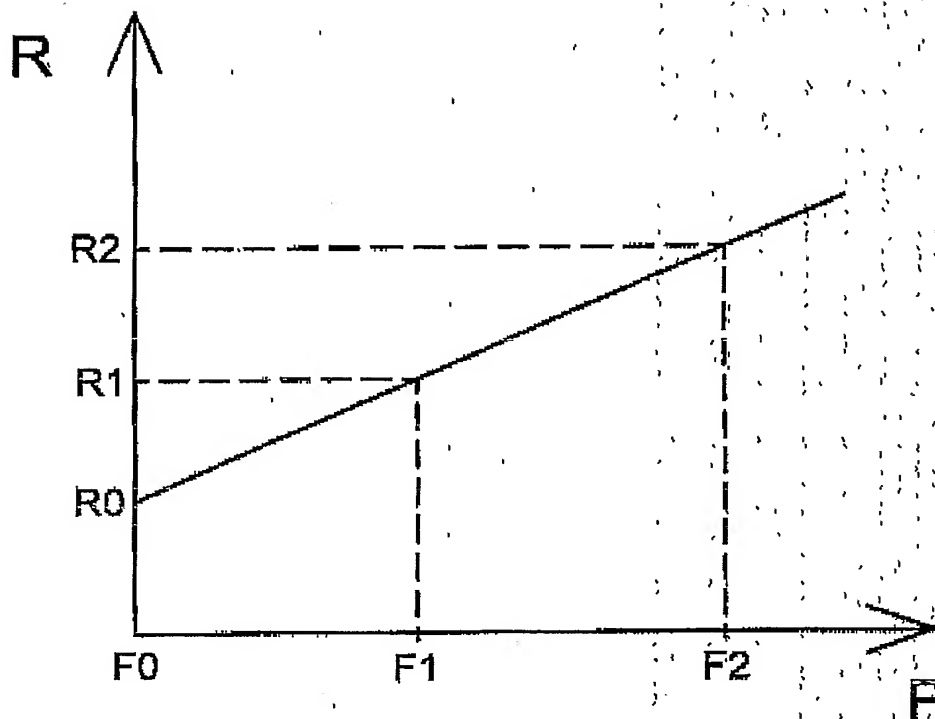


Fig 19



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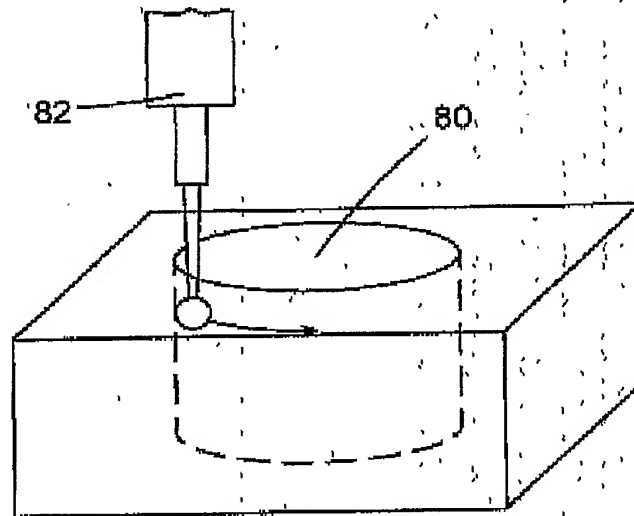


Fig 20

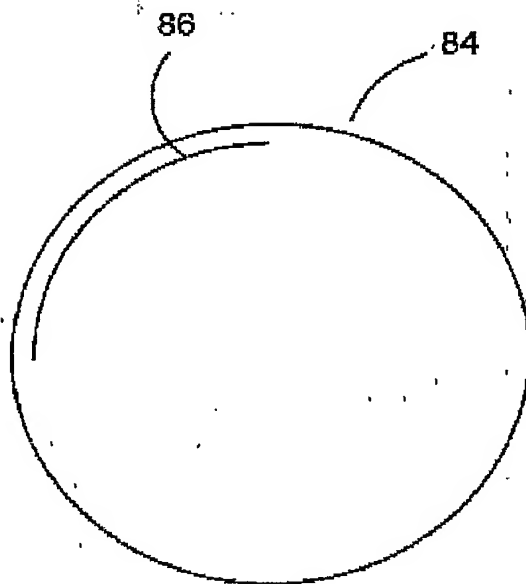


Fig 21

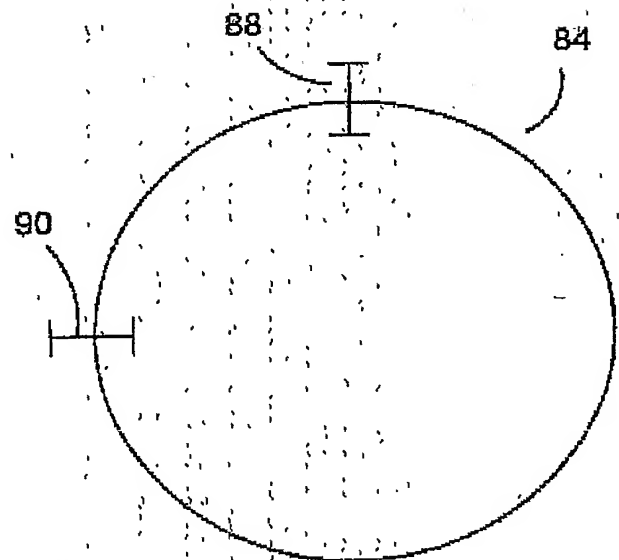
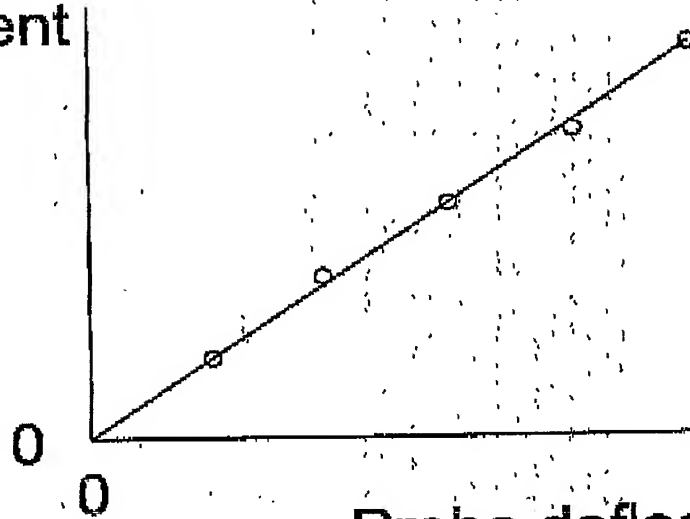


Fig 22



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Surface
measurement
error



Probe deflection/
Probe force

Fig 23

